

Client: Easy Signs Pty Ltd

**Project:** Design check – 2m × 2m Umbrella for 60km/hr Wind Speed

**Reference:** Easy Signs Technical Data

Report by: AL Checked by: EAB

Date: 27/03/2023

Amendment Date:

JOB No: D-1162

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1 Introduction

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Pty Ltd.

The report examines the effect of 3s gust wind of 60 km/hr on  $2m \times 2m$  Umbrella as the worst-case

scenario. The relevant Australian Standards AS1170.0:2002 General principles, AS1170.1:2002

Permanent, imposed, and other actions and AS1170.2:2021 Wind actions are used. The design check is

in accordance with AS/NZS 1664.2:1997 Aluminium Structures.

2 Design Restrictions and Limitations

2.1 The erected structure is for temporary use only.

2.2 It should be noted that if high gust wind speeds are anticipated or forecast in the locality of the tent, the

temporary erected structure should be dismantled.

2.3 For forecast winds in excess of (refer to summary) the structure should be completely folded.

(Please note that the locality squall or gust wind speed is affected by factors such as terrain exposure and

site elevations.)

2.4 The structure may only be erected in regions with wind classifications no greater than the limits specified on

the attached wind analysis.

2.5 The wind classifications are based upon category 2 in AS. Considerations have also been made to the

regional wind terrain category, topographical location and site shielding from adjacent structures. Please

note that in many instances topographical factors such as a location on the crest of a hill or on top of an

escarpment may yield a higher wind speed classification than that derived for a higher wind terrain category

in a level topographical region. For this reason, particular regard shall be paid to the topographical location

of the structure. For localities which do not conform to the standard prescribed descriptions for wind classes

as defined above, a qualified Structural Engineer may be employed to determine an appropriate wind class

for that the particular site.

2.6 The structures in no circumstances shall ever be erected in tropical or severe tropical cyclonic condition.

2.7 The tent structure has not been designed to withstand snow and ice loadings such as when erected in alpine

regions.

2.8 For the projects, where the site conditions approach the design limits, extra consideration should be given to

pullout tests of the stakes and professional assessment of the appropriate wind classification for the site.

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3 Specifications

3.1. General

Category	
Material	6063-T5

Size	Model
2m × 2m	Umbrella



\*base not included

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### 3.2. Section Properties

MEMBER(S)	Section	Section	b	d	t	Уc	$\mathbf{A}_{\mathbf{g}}$	$\mathbf{Z}_{\mathbf{x}}$	$\mathbf{Z}_{\mathrm{y}}$	S <sub>x</sub>	$\mathbf{S}_{\mathbf{y}}$	$\mathbf{I}_{\mathbf{x}}$	$\mathbf{I}_{\mathbf{y}}$	J	r <sub>x</sub>	r <sub>y</sub>
		mm	mm	mm	mm	$mm^2$	$mm^3$	$mm^3$	$mm^3$	$mm^3$	$mm^4$	$mm^4$	$mm^4$	mm	mm	
Scissor Beam	22x12x1	12	22	1	11.0	64.0	361.9	250.2	452.0	292.0	3981.3	1501.3	3335.1	7.9	4.8	
Upright Support	HEX 45x1	45	45	1	22.5	131.5	1350.0	1350.0	1670.0	1670.0	26400.0	26400.0	52700.0	14.2	14.2	

#### 4. Design Loads

#### 4.1. Ultimate

		Distributed load (kPa)	Design load factor (-)	Factored imposed load (kPa)
Live	Q	-	1.5	-
Self-weight	G	self-weight	1.35, 1.2, 0.9	1.2 self-weight, 0.9 self-weight
3s 60km/hr gust	W	0.138 C <sub>fig</sub>	1.0	$0.138C_{\mathrm{fig}}$

#### 4.2. Load Combinations

#### 4.2.1. Serviceability

Gravity =  $1.0 \times G$ 

Wind =  $1.0 \times G + 1.0 \times W$ 

#### 4.2.2. Ultimate

Downward =  $1.35 \times G$ 

=  $1.2 \times G + W_u$ 

Upward =  $0.9 \times G + W_u$ 

#### 5. Wind Analysis

Wind towards surface (+ve), away from surface (-ve)

#### 5.1. Parameters

Terrain category = 2

Site wind speed  $(V_{\text{sit,}\,\beta}) = V_R M_d (M_{z,\text{cat}} M_s M_t)$ 

 $V_R = 16.67 \text{ m/s} (60 \text{ km/hr})$ 

(regional 3 s gust wind speed)

 $M_d=1$ 

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 $M_s = 1$ 

 $M_t = 1$ 

 $M_{z,cat} = 0.91$  (Table 4.1(B) AS1170.2)

 $V_{sit,\beta}\!=15.17~m/s$ 

Height of structure (h) = 2.44 m (mid of peak and eave)

Width of structure (w) = 2 m

Length of structure (1) = 2 m

Pressure (P) =  $0.5\rho_{air} (V_{sit,\beta})^2 C_{fig} C_{dyn}$ 

 $= 0.138 C_{\rm fig} \ kPa$ 

Name	Symbol	Value	Unit	Notes	Ref.
			Input		
Importance level		2			Table 3.1 - Table 3.2 (AS1170.0)
Annual probability of exceedance		Temporary			Table 3.3
Regional gust wind speed		60	Km/hr		Table 3.1 (AS1170.2)
Regional gust wind speed	$V_R$	16.67	m/s		
Wind Direction Multipliers	$M_d$	1			Table 3.2 (AS1170.2)
Terrain Category Multiplier	$M_{Z,Cat}$	0.91			Table 4.1 (AS1170.2)
Shield Multiplier	Ms	1			4.3 (AS1170.2)
Topographic Multiplier	$M_t$	1			4.4 (AS1170.2)
Site Wind Speed	$V_{Site,\beta}$	15.17	m/s	$V_{Site,\beta} = V_R * M_d * M_{z,cat} * M_S, M_t$	
Pitch	α	18	Deg		
Pitch	α	0.31	rad		
Width	В	2	m		
Length	D	2	m		
Height	Z	2.44	m		
		W	ind Press	ure	
pair	ρ	1.2	Kg/m <sup>3</sup>		
dynamic response factor	$C_{dyn}$	1			
Wind Pressure	$ ho$ *C $_{fig}$	0.138	Kg/m <sup>2</sup>	$\rho$ =0.5 $\rho$ <sub>air</sub> *( $V$ <sub>des, <math>\beta</math></sub> ) <sup>2</sup> * $C$ <sub>fig</sub> * $C$ <sub>dyn</sub>	2.4 (AS1170.2)

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### 5.2. Pressure Coefficients ( $C_{fig}$ )

		WIND I	IRECTION 1	(θ=0)					
External Pressure									
4. Free Roof				α= <b>0</b> °					
Area Reduction Factor	Ka	1		u- <b>u</b>	D7				
local pressure factor	K <sub>i</sub>	1							
•		1							
porous cladding reduction factor  External Pressure Coefficient MIN	K <sub>p</sub>	-0.3							
External Pressure Coefficient MAX	C <sub>P,w</sub>	0.5							
	C <sub>P,w</sub>	-0.5							
External Pressure Coefficient MIN	C <sub>P,I</sub>								
External Pressure Coefficient MAX	C <sub>P,I</sub>	0							
aerodynamic shape factor MIN	$C_{fig,w}$	-0.30							
aerodynamic shape factor MAX	$C_{fig,w}$	0.50							
aerodynamic shape factor MIN	$C_{fig,I}$	-0.50							
aerodynamic shape factor MAX	$C_{fig,I}$	0.00							
Pressure Windward MIN	Р	-0.04	kPa						
Pressure Windward MAX	Р	0.07	kPa						
	_	-0.07	kPa						
Pressure Leeward MIN	Р	-0.07	NI G						
Pressure Leeward MIN Pressure Leeward MAX	P P	0.00	kPa						
		0.00		$\theta$ =90)					
		0.00	kPa						
Pressure Leeward MAX		0.00	kPa		D7				
Pressure Leeward MAX  4. Free Roof		0.00	kPa	e	D7				
	P	WIND DI	kPa	e	D7				
Pressure Leeward MAX  4. Free Roof Area Reduction Factor	P K <sub>a</sub> K <sub>i</sub>	0.00  WIND DI  Exte	kPa	e	D7				
Pressure Leeward MAX  4. Free Roof Area Reduction Factor local pressure factor	Р К <sub>а</sub> К <sub>і</sub> К <sub>р</sub>	WIND DI Exte	kPa	e	D7				
Pressure Leeward MAX  4. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor	К <sub>а</sub> К <sub>I</sub> К <sub>p</sub> С <sub>p,w</sub>	0.00  WIND DI  Exte	kPa	e	D7				
A. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN External Pressure Coefficient MAX	$\begin{matrix} K_a \\ K_l \\ K_p \\ C_{P,w} \\ C_{P,w} \end{matrix}$	0.00  WIND DI  Exte	kPa	e	D7				
A. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN External Pressure Coefficient MAX External Pressure Coefficient MIN	$\begin{matrix} K_a \\ K_l \\ K_p \\ C_{P,w} \\ C_{P,w} \\ C_{P,l} \end{matrix}$	0.00  WIND DI  Exte	kPa	e	D7				
4. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN	$\begin{matrix} K_a \\ K_l \\ K_p \\ C_{P,w} \\ C_{P,l} \\ C_{P,l} \end{matrix}$	0.00  WIND DI  Exte	kPa	e	D7				
4. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN External Pressure Coefficient MIN External Pressure Coefficient MIN External Pressure Coefficient MIN External Pressure Coefficient MAX aerodynamic shape factor MIN	$\begin{array}{c} K_a \\ K_l \\ K_p \\ C_{P,w} \\ C_{P,w} \\ C_{P,l} \\ C_{fig,w} \end{array}$	0.00  WIND DI Exte	kPa	e	D7				
A. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN External Pressure Coefficient MIN External Pressure Coefficient MIN External Pressure Coefficient MAX aerodynamic shape factor MIN aerodynamic shape factor MAX	$\begin{matrix} K_a \\ K_l \\ K_p \\ C_{P,w} \\ C_{P,l} \\ C_{P,l} \\ C_{fig,w} \\ C_{fig,w} \end{matrix}$	0.00  WIND DI Exte	kPa	e	D7				
A. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN External Pressure Coefficient MIN External Pressure Coefficient MAX External Pressure Coefficient MAX aerodynamic shape factor MIN aerodynamic shape factor MAX aerodynamic shape factor MIN	$\begin{array}{c} K_a \\ K_l \\ K_p \\ C_{P,w} \\ C_{P,w} \\ C_{P,l} \\ C_{fig,w} \\ C_{fig,w} \\ C_{fig,l} \end{array}$	0.00  WIND DI Exte	kPa	e	D7				
4. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN aerodynamic shape factor MIN	$\begin{array}{c} K_a \\ K_i \\ K_p \\ C_{P,w} \\ C_{P,i} \\ C_{P,i} \\ C_{fig,w} \\ C_{fig,w} \\ C_{fig,i} \\ C_{fig,i} \end{array}$	0.00  WIND DI Exter  1 1 1 -0.3 0.5 -0.5 0 -0.30 0.50 -0.50 0.00	RECTION 2 (	e	D7				
A. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN External Pressure Coefficient MIN External Pressure Coefficient MAX External Pressure Coefficient MAX aerodynamic shape factor MIN aerodynamic shape factor MAX	$\begin{array}{c} K_a \\ K_i \\ K_p \\ C_{P,w} \\ C_{P,i} \\ C_{P,i} \\ C_{fig,w} \\ C_{fig,i} \\ C_{fig,i} \\ \end{array}$	0.00  WIND DI Exter  1 1 1 -0.3 0.5 -0.5 0 -0.30 0.50 -0.50 0.00 -0.04	kPa  RECTION 2 ( ernal Pressure	e	D7				
A. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN aerodynamic shape factor MAX Pressure MIN (Windward Side) Pressure MAX (Windward Side)	$\begin{array}{c} K_a \\ K_i \\ K_p \\ C_{P,w} \\ C_{P,i} \\ C_{P,i} \\ C_{fig,w} \\ C_{fig,i} \\ C_{fig,i} \\ C_{fig,i} \\ \end{array}$	0.00  WIND DI Exter  1 1 1 -0.3 0.5 -0.5 0 -0.30 0.50 -0.50 0.00 -0.04 0.07	kPa  RECTION 2 ( ernal Pressure)	e	D7				
4. Free Roof Area Reduction Factor local pressure factor porous cladding reduction factor External Pressure Coefficient MIN	$\begin{array}{c} K_a \\ K_i \\ K_p \\ C_{P,w} \\ C_{P,i} \\ C_{P,i} \\ C_{fig,w} \\ C_{fig,i} \\ C_{fig,i} \\ \end{array}$	0.00  WIND DI Exter  1 1 1 -0.3 0.5 -0.5 0 -0.30 0.50 -0.50 0.00 -0.04	kPa  RECTION 2 ( ernal Pressure	e	D7				

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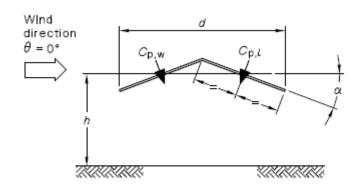
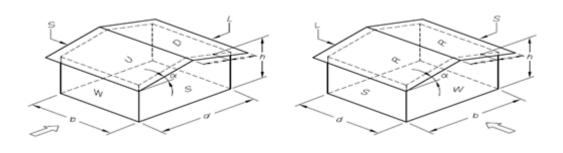


FIGURE D3 PITCHED FREE ROOFS



Direction 1 Direction 2

### 5.3. Pressure summary

WIND EXTERNAL PRESSURE	Direc	ction1	Direction2				
	Min (Kpa)	Max (Kpa)		Min (Kpa)	Max (Kpa)		
W	-0.04	0.07	W	-0.04	0.07		
L	-0.07	0.00	L	-0.07	0.00		

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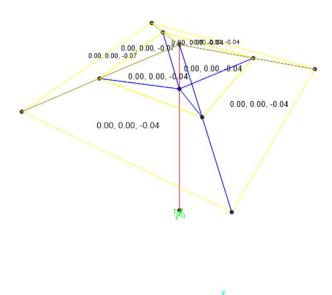
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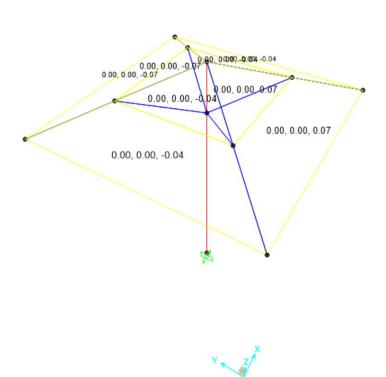
Web: www.cseds.com.au

### 5.4. Wind Load Diagrams

### 5.4.1. Wind 1 (kPa)



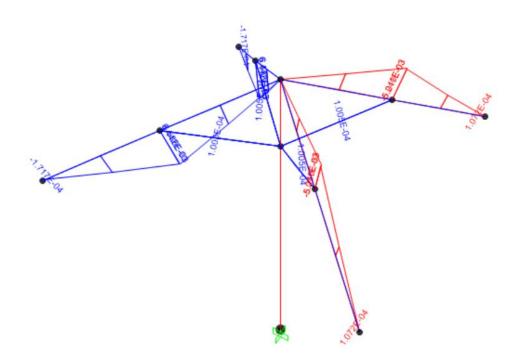
### 5.4.2. Wind 2 (kPa)



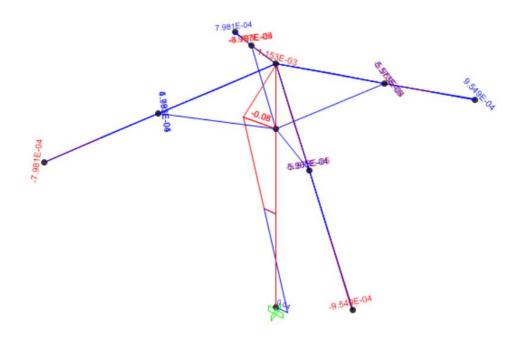
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### 5.4.3. Max Bending Moment due to critical load combination in major axis (kNm)



### 5.4.4. Max Bending Moment in minor axis due to critical load combination (kNm)



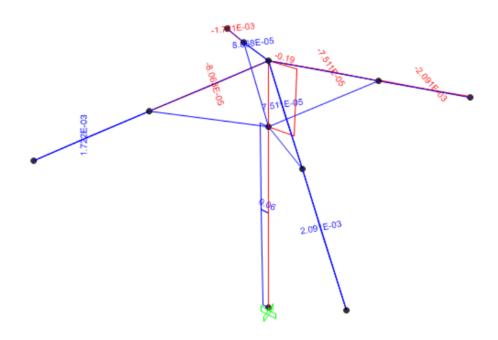
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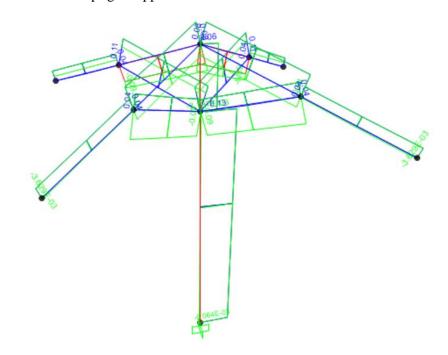
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#### 5.4.5. Max Shear in due to critical load combination (kN)



### 5.4.6. Max Axial force in upright support and roof beam due to critical load combination (kN)



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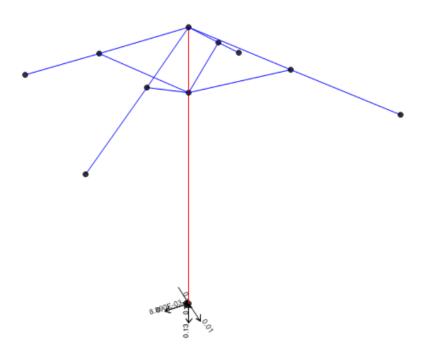
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### 5.4.7. Max reactions (kN)

N = 0.13 kN



### 6. Checking Members Based on AS/NZS 1664.2 Aluminium Structures

#### 6.1. Scissors Beams

NAME	SYMBOL		VALUE	UNI T	NOTES	REF
22x12x1	Scissor Beam					
Alloy and temper	6063-T5					AS1664.1
	Ftu	=	152	MPa	Ultimate	T3.3(A)
Tension	$F_{ty}$	=	110	MPa	Yield	
Compression	F <sub>cy</sub>	=	110	MPa		
Shear	Fsu	=	90	MPa	Ultimate	
Sileai	$F_{sy}$	=	62	MPa	Yield	
Pooring	F <sub>bu</sub>	=	62	MPa	Ultimate	
Bearing	$F_by$	=	179	MPa	Yield	
Modulus of elasticity	E	=	70000	MPa	Compressiv e	

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	k <sub>t</sub> k <sub>c</sub>	=	1 1			T3.4(B)
FEM ANALYSIS RESULTS						
Axial force	Р	=	0.086	kN	compressio n	
	Р	=	0	kN	Tension	
In plane moment	$M_{x}$	=	0.0064	kNm		
Out of plane moment	$M_{y}$	=	0	kNm		
DESIGN STRESSES						
Gross cross section area	Ag	=	64	mm²		
In-plane elastic section modulus	$Z_{x}$	=	361.9393 9	mm³		
Out-of-plane elastic section mod.	$Z_{y}$	=	250.2222 2	mm³		
Stress from axial force	fa	=	P/A <sub>g</sub>			
		=	1.34	MPa	compressio n	
		=	0.00	MPa	Tension	
Stress from in-plane bending	$\mathbf{f}_{\mathbf{bx}}$	=	$M_x/Z_x$			
		=	17.68	MPa	compressio n	
Stress from out-of-plane	$\mathbf{f}_{\mathbf{by}}$	=	$M_y/Z_y$			
bending		=	0.00	MPa	compressio n	
Tension						
3.4.3 Tension in rectangular tubes						
	фГ∟	=	104.50	MPa		
		O R				
	φFL	=	129.20	MPa		
COMPRESSION						
3.4.8 Compression in columns, axi	al, gross se	ction				
1. General						3.4.8.1

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buckling axis (X)  Slenderness ratio $kLb/ry = 306.40$ Slenderness ratio $kL/rx = 188.15$ Slenderness parameter $\lambda = 3.866$ $D_c^* = 39.0$ $S_1^* = 0.24$ $S_2^* = 1.25$ $\phi_{cc} = 0.950$ Factored limit state stress $\phi F_L = 6.99$ $\phi F_L = 6.9$
Slenderness ratio $kLb/ry = 306.40$ Slenderness ratio $kL/rx = 188.15$ Slenderness parameter $\lambda = 3.866$ $D_c^* = 39.0$ $S_1^* = 0.24$ $S_2^* = 1.25$ $\phi_{cc} = 0.950$ Factored limit state stress $\phi$ F <sub>L</sub> = 6.99 MPa
Slenderness ratio kLb/ry = 306.40 Slenderness ratio kL/rx = 188.15 $ \begin{array}{ccccccccccccccccccccccccccccccccccc$
Slenderness ratio kLb/ry = 306.40 Slenderness ratio kL/rx = 188.15 $ \begin{array}{ccccccccccccccccccccccccccccccccccc$
Slenderness ratio $kLb/ry = 306.40$ Slenderness ratio $kL/rx = 188.15$ Slenderness parameter $\lambda = 3.866$ $D_c^* = 39.0$
Slenderness ratio kLb/ry = 306.40
buckling axis (A)
buckling axis (Y) $r_y = 4.84$ mm  Radius of gyration about $r_x = 7.89$ mm
Unsupported length of member L = 1484 mm  Effective length factor k = 1.00  Radius of gyration about

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Most adverse tensile limit state stress	Fa	=	104.50	MPa		
Most adverse compressive & Tensile capacity factor	f <sub>a</sub> /F <sub>a</sub>	=	0.19		PASS	
BENDING - IN-PLANE						
3.4.15 Compression in beams, extrubes, box sections	reme fibre, g	gross se	ection rectan	gular		
Unbraced length for bending	$L_b$	=	1484	mm		
Second moment of area (weak axis)	ly	=	1.50E+03	mm <sup>4</sup>		
Torsion modulus	J	=	3.34E+03	$\rm mm^3$		
Elastic section modulus	Z	=	361.9393 9	mm³		
Slenderness	S	=	480.08			
Limit 1	S <sub>1</sub>	=	21.80			
Limit 2	S <sub>2</sub>	=	3854.05			
Factored limit state stress	φF <sub>L</sub>	=	86.70	MPa		3.4.15(2)
<b>3.4.17</b> Compression in component uniform compression), gross section supported						
.,	<b>k</b> 1	=	0.5			T3.3(D)
	$k_2$	=	2.04			T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	10	mm		
	t	=	1	mm		
Slenderness	b/t	=	10			
Limit 1	S <sub>1</sub>	=	12.06			
Limit 2	$S_2$	=	71.35			
Factored limit state stress	фГ∟	=	104.50	MPa		
Most adverse in-plane bending limit state stress	F <sub>bx</sub>	=	86.70	MPa		

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Most adverse in-plane bending capacity factor	$f_{bx}/F_{bx}$	=	0.20		PASS	
BENDING - OUT-OF-PLANE						
NOTE: Limit state stresses, φF <sub>L</sub> at (doubly symmetric section)	re the same t	for out-o	f-plane ber	nding		
Factored limit state stress	фF∟	=	86.70	MPa		
Most adverse out-of-plane bending limit state stress	F <sub>by</sub>	=	86.70	MPa		
Most adverse out-of-plane bending capacity factor	f <sub>by</sub> /F <sub>by</sub>	=	0.00		PASS	
COMBINED ACTIONS						
4.1.1 Combined compression and	bending					4.1.1(2)
	Fa	=	6.99	MPa		3.4.8
	Fao	=	104.50	MPa		3.4.10
	$F_{bx}$	=	86.70	MPa		3.4.17
	$F_by$	=	86.70	MPa		3.4.17
	f <sub>a</sub> /F <sub>a</sub>	=	0.192			
Check:	$f_a/F_a + f_{bx}/F_{bx}$	+ f <sub>by</sub> /F <sub>by</sub>	≤ 1.0			4.1.1
i.e.,	0.40	≤	1.0		PASS	
SHEAR		_		_		
3.4.24 Shear in webs (Major						4.1.1(2)
Axis)						4.1.1(2)
Clear web height	h	=	20	mm		
	t	=	1	mm		
Slenderness	h/t	=	20			
Limit 1	S <sub>1</sub>	=	33.38			
Limit 2	S <sub>2</sub>	=	59.31			
Factored limit state stress	φF <sub>L</sub>	=	58.90	MPa		

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Stress From Shear force	$f_{sx}$	=	$V/A_w$			
3.4.25 Shear in webs (Minor Axis)			0.00	MPa		
Clear web height	b	=	10	mm		
	t	=	1	mm		
Slenderness	b/t	=	10			
Factored limit state stress	φFL	=	58.90	MPa		
Stress From Shear force	$\mathbf{f}_{sy}$	=	$V/A_w$			
			0.18	MPa		
Martalananalananan						
Most adverse shear capacity factor (Major Axis)	$f_{sx}/F_{sx}$	=	0.00	MPa		
Most adverse shear capacity factor (Minor Axis)	f <sub>sy</sub> /F <sub>sy</sub>	=	0.00	MPa	PASS	
COMBINED ACTIONS		_		_		
	on and handin	.~				
<b>4.4</b> Combined Shear, Compression	nı anu bendiri	y				
Check:	$f_a/F_a + f_b/F_b +$	(f <sub>s</sub> /F <sub>s)</sub> <sup>2</sup> ≤	≤ 1.0			
i.e.,	0.40	≤	1.0		PASS	

### 6.2. Upright Support

NAME	SYMBOL		VALUE	UNI T	NOTES	REF
HEX 45x1	Upright Support					
Alloy and temper	6063-T5					AS1664.1
Tension	$F_tu$	=	152	MPa	Ultimate	T3.3(A)
Tension	$F_{ty}$	=	110	MPa	Yield	
Compression	F <sub>cy</sub>	=	110	MPa		
Shear	$F_su$	=	90	MPa	Ultimate	
Sileai	F <sub>sy</sub>	=	62	MPa	Yield	
Bearing	F <sub>bu</sub>	=	62	MPa	Ultimate	

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	$F_{by}$	=	179	MPa	Yield	
Modulus of elasticity	Е	=	70000	MPa	Compressiv e	
	$\mathbf{k}_{t}$	=	1			To 4(D)
	<b>k</b> <sub>c</sub>	=	1			T3.4(B)
FEM ANALYSIS RESULTS						
Axial force	Р	=	0	kN	compressio n	
	Р	=	0.131	kN	Tension	
In plane moment	$M_{x}$	=	0.0839	kNm		
Out of plane moment	$M_{y}$	=	0	kNm		
DESIGN STRESSES						
Gross cross section area	Ag	=	131.5	mm <sup>2</sup>		
In-plane elastic section modulus	$Z_{x}$	=	1350	mm³		
Out-of-plane elastic section mod.	Zy	=	1350	mm³		
Stress from axial force	fa	=	P/A <sub>g</sub>			
		=	0.00	MPa	compressio n	
		=	1.00	MPa	Tension	
Stress from in-plane bending	$\mathbf{f}_{bx}$	=	$M_x/Z_x$			
		=	62.15	MPa	compressio n	
Stress from out-of-plane	$\mathbf{f}_{by}$	=	$M_y/Z_y$			
bending		=	0.00	MPa	compressio n	
Tension						
3.4.3 Tension in rectangular tubes						
	φF∟	=	104.50	MPa		
		O R				
	φF∟	=	129.20	MPa		

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COMPRESSION					
3.4.8 Compression in columns, a	xial, gross sect	tion			
1. General					3.4.8.1
Unsupported length of member	L	=	2440	mm	
Effective length factor	k	=	1.00		
Radius of gyration about buckling axis (Y)	r <sub>y</sub>	=	14.17	mm	
Radius of gyration about buckling axis (X)	r <sub>x</sub>	=	14.17	mm	
Slenderness ratio	kLb/ry	=	172.21		
Slenderness ratio	kL/rx	=	172.21		
Classican and an arrangement	,		0.47		
Slenderness parameter	λ	=	2.17		
	D <sub>c</sub> *	=	39.0		
	S <sub>1</sub> *	=	0.24		
	S <sub>2</sub> *	=	1.25		
	фсс	=	0.884		
Factored limit state stress	φF <sub>L</sub>	=	20.60	МРа	
2. Sections not subject to torsion	al or torsional-f	lexural l	ouckling		3.4.8.2
Largest slenderness ratio for flexural buckling	kL/r	=	172.21		
3.4.10 Uniform compression in coflat plates	omponents of c	olumns,	gross sec	tion -	
Uniform compression in composites with both edges supported		nns, gro	ss section	- flat	3.4.10.1
	<b>k</b> <sub>1</sub>	=	0.35		T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	43		
	t	=	1	mm	
Slenderness	b/t	=	43		
Limit 1	S <sub>1</sub>	=	12.06		
				1	

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Factored limit state stress	φF∟	=	79.75	MPa		
Most adverse compressive limit state stress	Fa	=	20.60	MPa		
Most adverse tensile limit state stress	Fa	=	104.50	MPa		
Most adverse compressive & Tensile capacity factor	f <sub>a</sub> /F <sub>a</sub>	=	0.01		PASS	
BENDING - IN-PLANE						
<b>3.4.15</b> Compression in beams, ex tubes, box sections	treme fibre, g	ross sec	tion rectang	gular		
Unbraced length for bending	$L_b$	=	2440	mm		
Second moment of area (weak axis)	ly	=	2.64E+0 4	mm <sup>4</sup>		
Torsion modulus	J	=	5.27E+0 4	mm³		
Elastic section modulus	Z	=	1350	${\rm mm^3}$		
Slenderness	S	=	176.62			
Limit 1	$S_1$	=	21.80			
Limit 2	S <sub>2</sub>	=	3854.05			
Factored limit state stress	фF∟	=	92.48	MPa		3.4.15(2)
3.4.17 Compression in componen compression), gross section - flat						
, , ,	<b>k</b> 1	=	0.5			T3.3(D)
	$k_2$	=	2.04			T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	43	mm		
•	t	=	1	mm		
Slenderness	b/t	=	43			
Limit 1	S <sub>1</sub>	=	12.06			
Limit 2	S <sub>2</sub>	=	71.35			
					ı	1

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Most adverse in-plane bending limit state stress	F <sub>bx</sub>	=	79.75	MPa		
Most adverse in-plane bending capacity factor	$f_{bx}/F_{bx}$	=	0.78		PASS	
BENDING - OUT-OF-PLANE						
NOTE: Limit state stresses, φF <sub>L</sub> a (doubly symmetric section)	re the same fo	r out-of-	plane ben	ding		
Factored limit state stress	φFL	=	79.75	MPa		
Most adverse out-of-plane bending limit state stress	F <sub>by</sub>	=	79.75	MPa		
Most adverse out-of-plane bending capacity factor	f <sub>by</sub> /F <sub>by</sub>	=	0.00		PASS	
COMBINED ACTIONS						
4.1.1 Combined compression and	bending					4.1.1(2)
	Fa	=	20.60	MPa		3.4.8
	Fao	=	79.75	MPa		3.4.10
	$F_bx$	=	79.75	MPa		3.4.17
	$F_{by}$	=	79.75	MPa		3.4.17
	f <sub>a</sub> /F <sub>a</sub>	=	0.010			
Check: 1	$a/F_a + f_{bx}/F_{bx} +$	f <sub>by</sub> /F <sub>by</sub> ≤	1.0			4.1.1
i.e.,	0.79	≤	1.0		PASS	
SHEAR						
<b>3.4.24</b> Shear in webs (Major Axis)						4.1.1(2)
Clear web height	h	=	43	mm		
	t	=	1	mm		
Slenderness	h/t	=	43			
Limit 1	$S_1$	=	33.38			

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Factored limit state stress	φF <sub>L</sub>	=	56.20	MPa	
Stress From Shear force	$f_{sx}$	=	$V/A_w$		
			0.00	MPa	
3.4.25 Shear in webs (Minor					
Axis)					
Clear web height	b	=	43	mm	
Ü	t	=	1	mm	
Slenderness	b/t	=	43		
Factored limit state stress	φF <sub>L</sub>	=	56.20	MPa	
Stress From Shear force	$\mathbf{f}_{sy}$	=	$V/A_w$		
			1.70	MPa	
Most adverse shear capacity factor (Major Axis)	$f_{sx}/F_{sx}$	=	0.00	MPa	
Most adverse shear capacity factor (Minor Axis)	$f_{sy}/F_{sy}$	=	0.03	MPa	PASS
COMBINED ACTIONS					
4.4 Combined Shear, Compress	ion and bending	7			
Check:	$f_a/F_a + f_b/F_b + (f_a/F_a)$		1.0		
i.e.,	0.79	≤	1.0		PASS

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### 7. Summary and conclusions

- a. The  $2m \times 2m$  Umbrella as specified has been analyzed with a conclusion that it has the capacity to withstand wind speeds up to and including 60km/hr.
- b. For forecast winds in excess of **60km/hr** the structure should be completely folded.
- c. For uplift due to 60km/hr, 0.13 kN (13kg) holding down weight for upright support is required.
- d. The bearing pressure of soil should be clarified and checked by an engineer prior to any construction for considering foundation and base plate.

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e. Design of fabric is by others.

Yours faithfully,

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